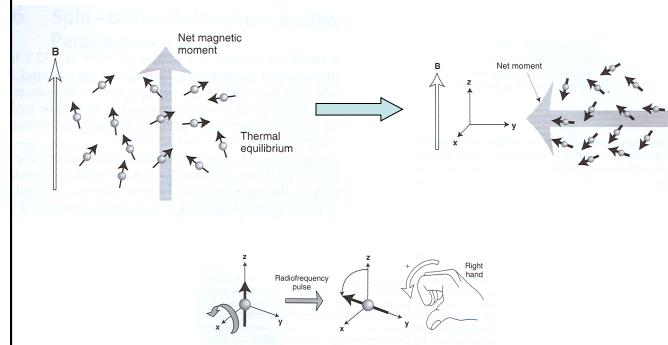


Bioengineering 280A  
Principles of Biomedical Imaging

Fall Quarter 2015  
MRI Lecture 6

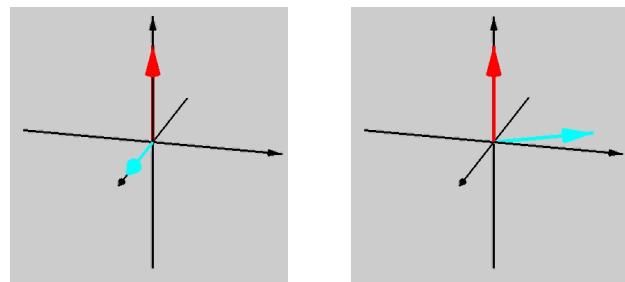
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## RF Excitation



From Levitt, Spin Dynamics, 2001

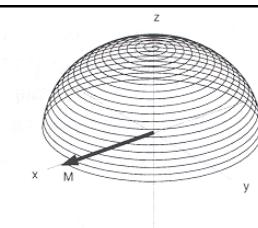
## RF Excitation



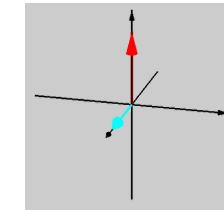
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<http://www.eecs.umich.edu/%7Ednol/BME516/>

a) Laboratory frame behavior of  $\mathbf{M}$   
Images & caption: Nishimura, Fig. 3.3

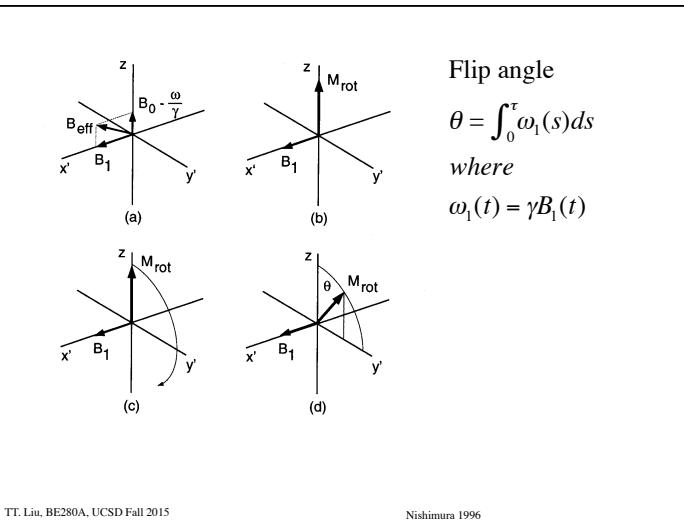


b) Rotating frame behavior of  $\mathbf{M}$



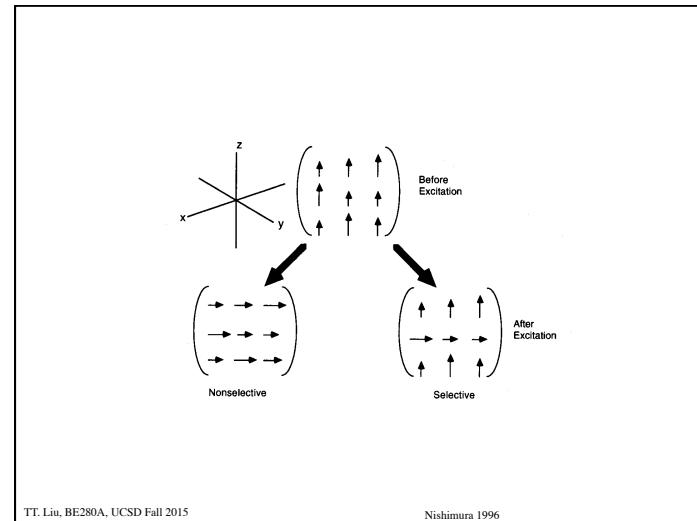
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<http://www.eecs.umich.edu/%7Ednol/BME516/>



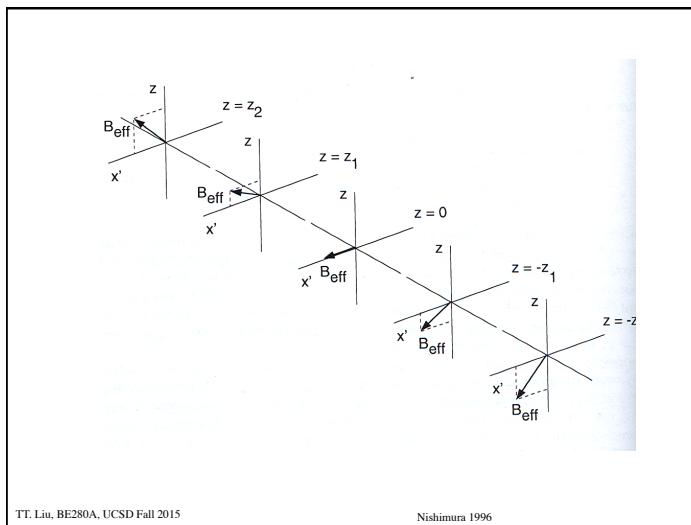
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Nishimura 1996



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Nishimura 1996



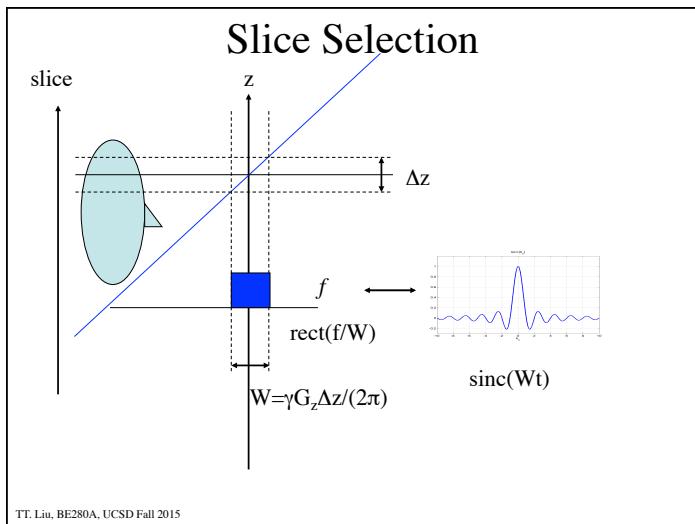
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Nishimura 1996

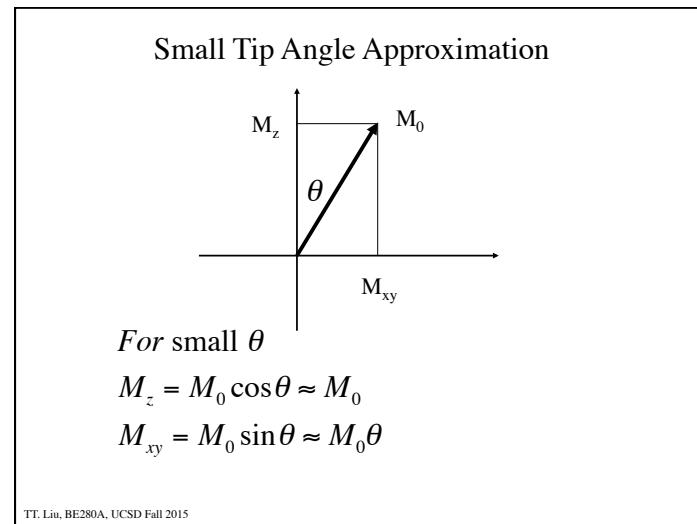


<https://www.youtube.com/watch?v=kODOL-QBzM>

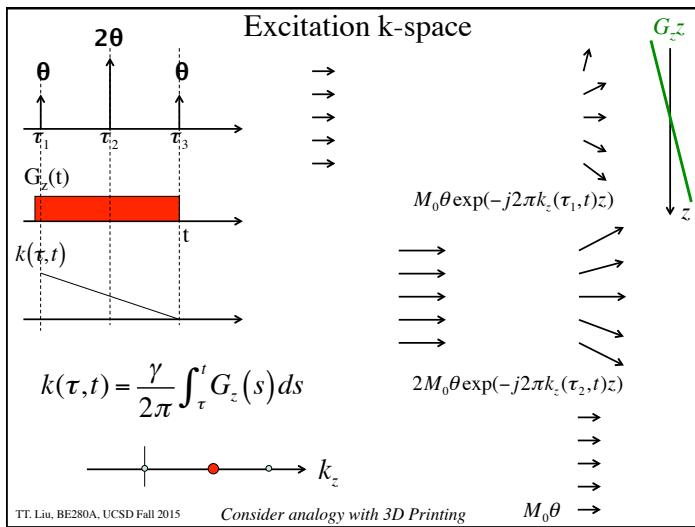
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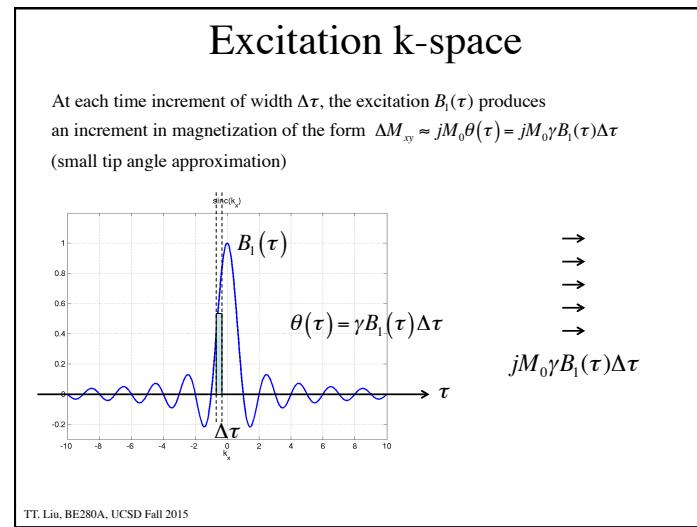
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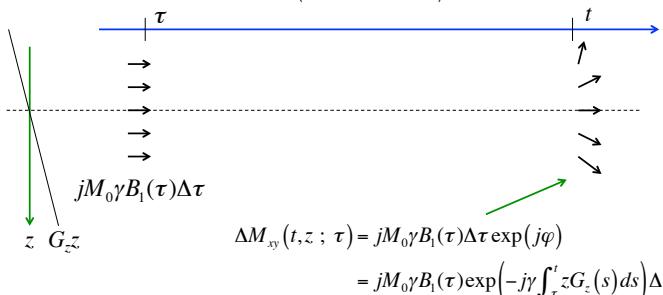
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## Excitation k-space

In the presence of a gradient, this will accumulate phase of the form

$$\varphi = -\gamma \int_{\tau}^t z G_z(s) ds, \text{ such that the incremental magnetization at time } t \text{ is}$$

$$\Delta M_{xy}(t, z; \tau) = jM_0 \gamma B_l(\tau) \exp\left(-j\gamma \int_{\tau}^t z G_z(s) ds\right) \Delta \tau$$



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## Excitation k-space

Integrating over all time increments  $d\tau$ , we obtain

$$M_{xy}(t, z) = jM_0 \int_{-\infty}^t \gamma B_l(\tau) \exp\left(-j\gamma \int_{\tau}^t z G_z(s) ds\right) d\tau$$

$$= jM_0 \int_{-\infty}^t \gamma B_l(\tau) \exp(-j2\pi k(\tau, t)z) d\tau$$

$$\text{where } k(\tau, t) = \frac{\gamma}{2\pi} \int_{\tau}^t G_z(s) ds$$

This has the form of a Fourier transform, where we are integrating the contributions of the field  $B_l(\tau)$  at the k-space point  $k(\tau, t)$ .

For a historical perspective see

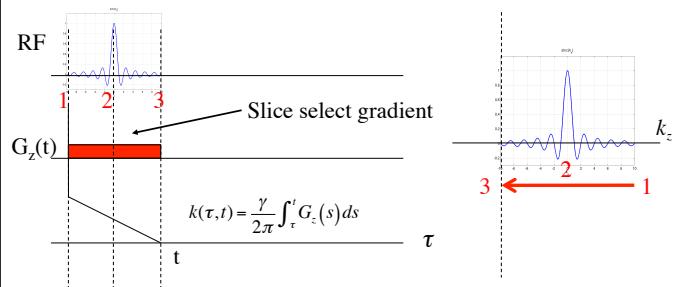
<http://www.sciencedirect.com/science/article/pii/S1090780711002655>

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## Excitation k-space

$$M_{xy}(t, z) = jM_0 \int_{-\infty}^t \gamma B_l(\tau) \exp(-j2\pi k(\tau, t)z) d\tau$$

This has the form of a Fourier transform, where we are integrating the contributions of the field  $B_l(\tau)$  at the k-space point  $k(\tau, t)$ .

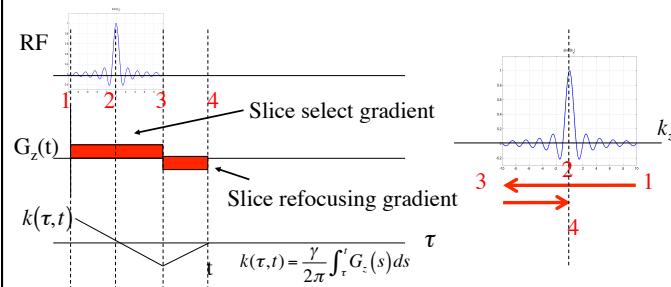


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## Refocusing

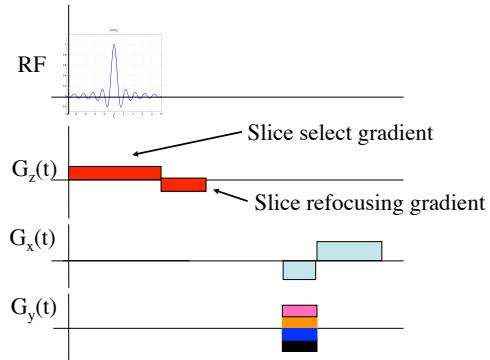
$$M_{xy}(t, z) = jM_0 \int_{-\infty}^t \gamma B_l(\tau) \exp(-j2\pi k(\tau, t)z) d\tau$$

This has the form of a Fourier transform, where we are integrating the contributions of the field  $B_l(\tau)$  at the k-space point  $k(\tau, t)$ .



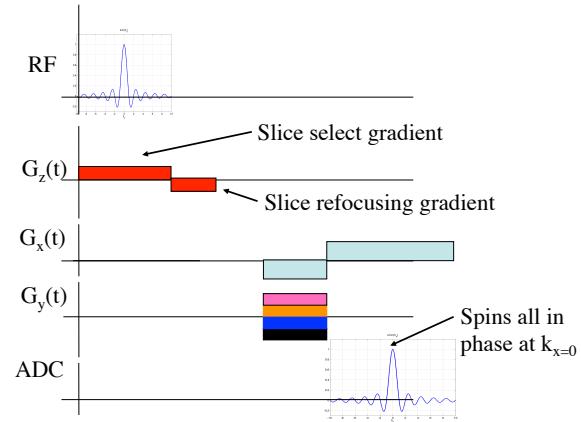
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## Slice Selection

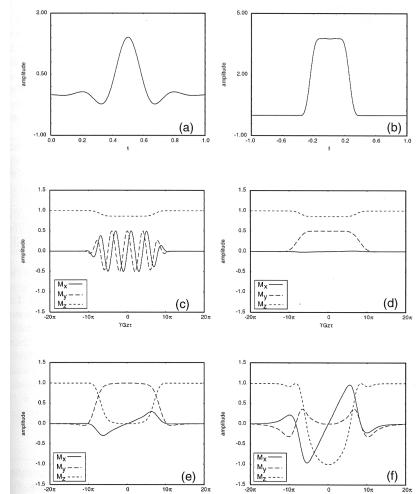


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## Gradient Echo



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### Example

$$M_{xy}(x) = M_0 \cos(4\pi x)$$

$$F(M_{xy}(x)) = \frac{M_0}{2} (\delta(k_x - 2) + \delta(k_x + 2))$$

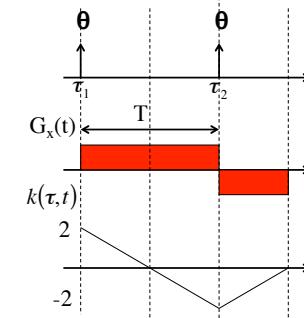
$$g_{\max} = 4 \text{ G/cm}$$

$$\frac{\gamma}{2\pi} g_{\max} T = 4 \text{ cm}^{-1}; \quad T = 235 \mu\text{sec}$$

$$\text{with small tip angle approximation} \rightarrow \theta = \frac{1}{2}$$

$$\text{Compare with } \sin\left(\frac{\pi}{6}\right) = \frac{1}{2} \rightarrow \theta = \frac{\pi}{6} = 0.5236$$

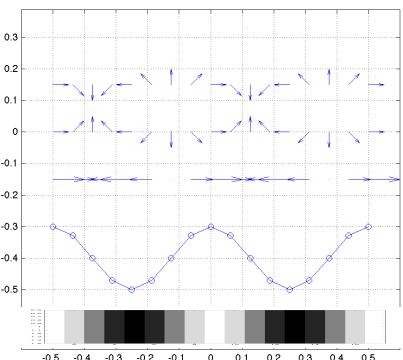
Question: Should we use  $\theta = \frac{\pi}{4}$  instead?



Exercise: Sketch the quiver diagrams corresponding to the contributions of the two RF pulses and show that they produce the desired pattern.

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Exercise: Sketch the quiver diagrams corresponding to the contributions of the two RF pulses and show that they produce the desired pattern. (Patterns shown below scaled for display purposes)



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## Slice Selection Problem

Consider a desired slice profile of the form  $m(z) = M_0 \text{rect}(z/(10\text{mm}))$ .

You are given an RF pulse of the form  $p(t) = A \cdot \text{sinc}\left(\frac{t}{T}\right)$

where  $T = 400 \mu\text{sec}$

(1) What amplitude gradient should you use to achieve the desired slice profile?

*HINT:* Think about where the first zero in  $k_z$  space must appear. Then think about what gradient is needed so that the first zero in the RF occurs at the desired location in  $k$ -space. An alternate approach is to consider the frequency range of the spins that need to be excited within the slice and also consider the bandwidth of the RF pulse.

(2) What should the amplitude  $A$  of the RF pulse be?

(3) What happens to the slice profile if you truncate the RF pulse to have a duration of 3.2 ms?

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## Time-Bandwidth Product (TBW)

$$\text{sinc}\left(\frac{t}{\tau}\right)\text{rect}\left(\frac{t}{2N\tau}\right) \Rightarrow \text{rect}(\tau f) * 2N\tau \text{sinc}(2N\tau f)$$

Duration =  $2N\tau$

$$\text{Bandwidth} = \frac{1}{\tau} \Rightarrow \Delta z = \frac{2\pi}{\gamma G_z \tau}$$

$$\text{Transition Width} \approx \frac{1}{2N\tau} \Rightarrow \Delta z' = \frac{2\pi}{\gamma G_z 2N\tau}$$

$$\text{Time - Bandwidth Product (TBW)} = 2N\tau \frac{1}{\tau} = 2N$$

$$\text{also, TBW} = \frac{\text{Bandwidth}}{\text{Transition Width}}$$

For a fixed duration pulse, we can increase TBW by increasing the Bandwidth.

(Note : this will also lead to an increase in N).

This will require a higher B1 amplitude and a higher gradient to keep the slice width constant -- note that with higher TBW the physical transition width then decreases.

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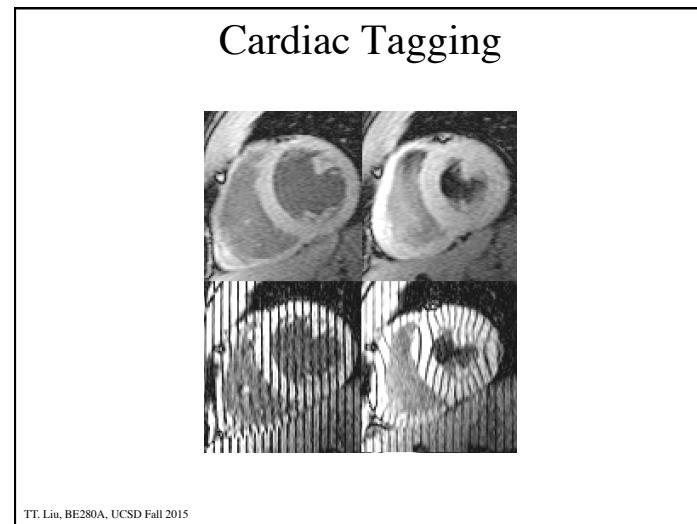
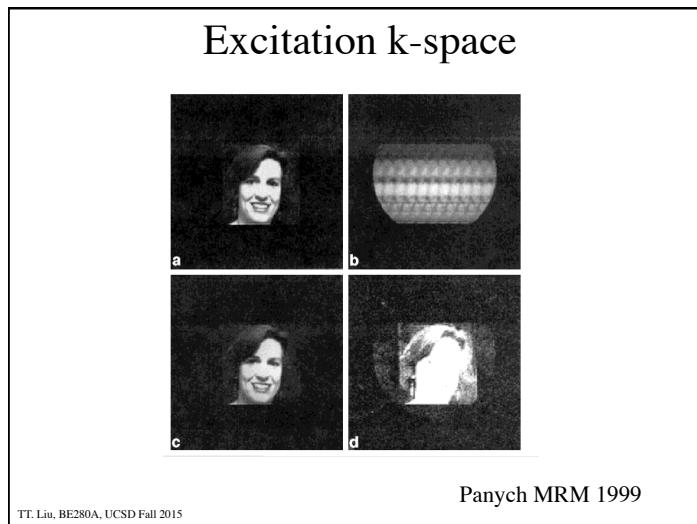
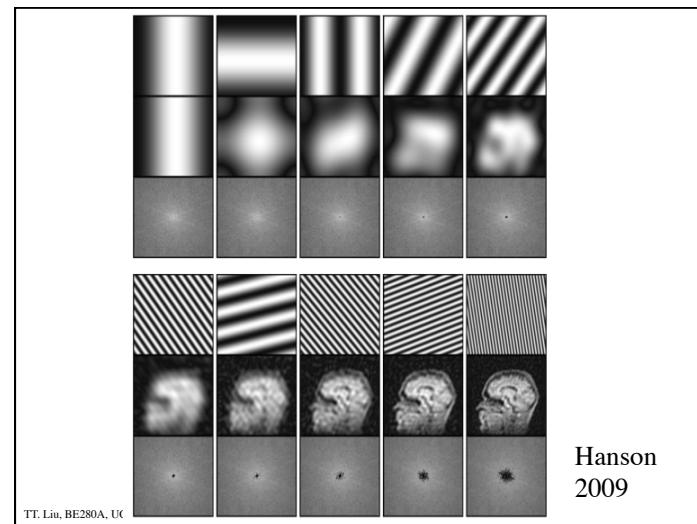
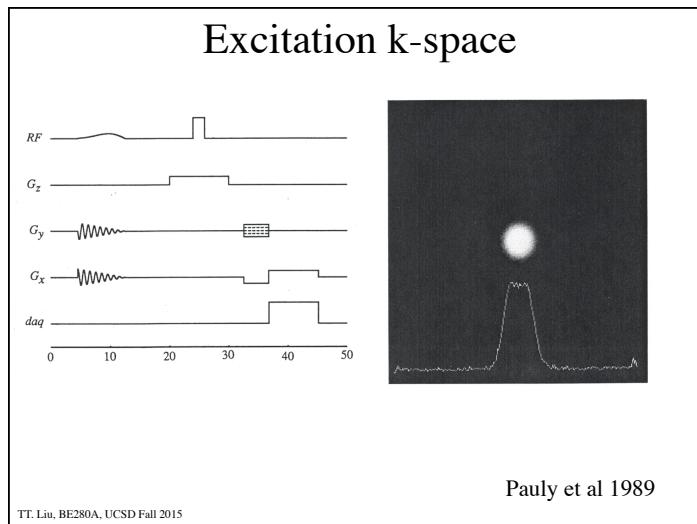
## Multi-dimensional Excitation $k$ -space

$$M_{xy}(t, \mathbf{r}) = jM_0 \int_{-\infty}^t \omega_1(\tau) \exp\left(-j\gamma \int_{\tau}^t \mathbf{G}(s) \cdot \mathbf{r} ds\right) d\tau \\ = jM_0 \int_{-\infty}^t \omega_1(\tau) \exp(j2\pi \mathbf{k}(\tau) \cdot \mathbf{r}) d\tau$$

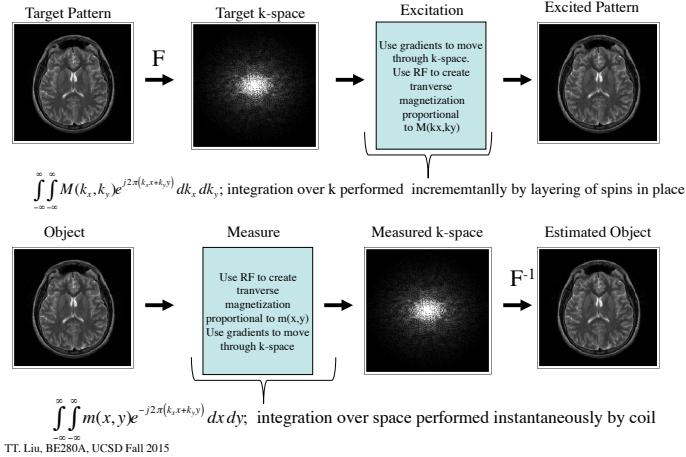
$$\text{where } \mathbf{k}(\tau) = -\frac{\gamma}{2\pi} \int_{\tau}^t \mathbf{G}(t') dt'$$

Pauly et al 1989

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## Imaging and Excitation



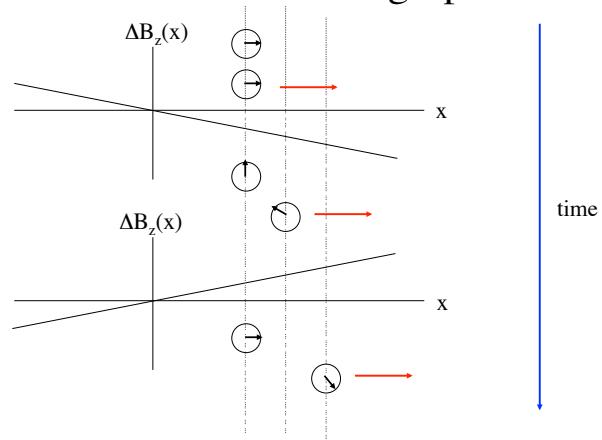
## Moving Spins (preview)

So far we have assumed that the spins are not moving (aside from thermal motion giving rise to relaxation), and contrast has been based upon  $T_1$ ,  $T_2$ , and proton density. We were able to achieve different contrasts by adjusting the appropriate pulse sequence parameters.

Biological samples are filled with moving spins, and we can also use MRI to image the movement. Examples: blood flow, diffusion of water in the white matter tracts. In addition, we can also sometimes induce motion into the object to image its mechanical properties, e.g. imaging of stress and strain with MR elastography.

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## Phase of Moving Spin



## Phase of a Moving Spin

$$\begin{aligned}\varphi(t) &= - \int_0^t \Delta\omega(\tau) d\tau \\ &= - \int_0^t \gamma \Delta B(\tau) d\tau \\ &= - \int_0^t \gamma \vec{G}(\tau) \cdot \vec{r}(\tau) d\tau \\ &= - \gamma \int_0^t [G_x(\tau)x(\tau) + G_y(\tau)y(\tau) + G_z(\tau)z(\tau)] d\tau\end{aligned}$$

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## Phase of Moving Spin

Consider motion along the x-axis

$$x(t) = x_0 + vt + \frac{1}{2}at^2$$

$$\begin{aligned}\varphi(t) &= -\gamma \int_0^t G_x(\tau)x(\tau)d\tau \\ &= -\gamma \int_0^t G_x(\tau) \left[ x_0 + v\tau + \frac{1}{2}a\tau^2 \right] d\tau \\ &= -\gamma \left[ x_0 \int_0^t G_x(\tau)d\tau + v \int_0^t G_x(\tau)\tau d\tau + \frac{a}{2} \int_0^t G_x(\tau)\tau^2 d\tau \right] \\ &= -\gamma \left[ x_0 M_0 + vM_1 + \frac{a}{2} M_2 \right]\end{aligned}$$

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## Phase of Moving Spin

$$\varphi(t) = -\gamma \left[ x_0 M_0 + vM_1 + \frac{a}{2} M_2 \right]$$

$$M_0 = \int_0^t G_x(\tau)d\tau$$

Zeroth order moment

$$M_1 = \int_0^t G_x(\tau)\tau d\tau$$

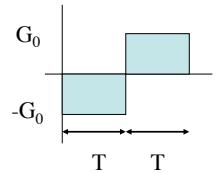
First order moment

$$M_2 = \int_0^t G_x(\tau)\tau^2 d\tau$$

Second order moment

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## Flow Moment Example

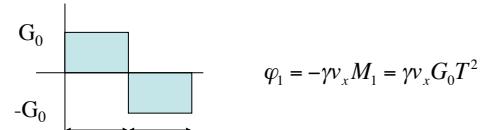


$$M_0 = \int_0^t G_x(\tau)d\tau = 0$$

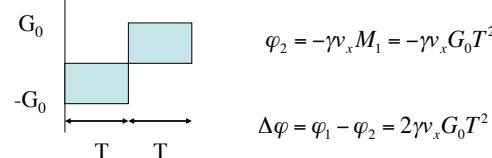
$$\begin{aligned}M_1 &= \int_0^t G_x(\tau)\tau d\tau \\ &= -\int_0^T G_0 \tau d\tau + \int_T^{2T} G_0 \tau d\tau \\ &= G_0 \left[ -\frac{\tau^2}{2} \Big|_0^T + \frac{\tau^2}{2} \Big|_T^{2T} \right] \\ &= G_0 \left[ -\frac{T^2}{2} + \frac{4T^2}{2} - \frac{T^2}{2} \right] = G_0 T^2\end{aligned}$$

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## Phase Contrast Angiography (PCA)



$$\varphi_1 = -\gamma v_x M_1 = \gamma v_x G_0 T^2$$



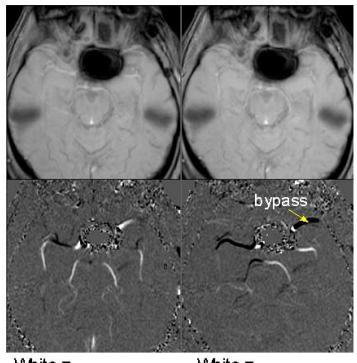
$$\varphi_2 = -\gamma v_x M_1 = -\gamma v_x G_0 T^2$$

$$\Delta\varphi = \varphi_1 - \varphi_2 = 2\gamma v_x G_0 T^2$$

$$v_x = \frac{\Delta\varphi}{2G_0 T^2}$$

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## PCA example



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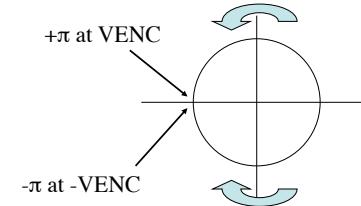
[http://www.medical.philips.com/main/products/mri/assets/images/case\\_of\\_week/cow\\_51\\_s5.jpg](http://www.medical.philips.com/main/products/mri/assets/images/case_of_week/cow_51_s5.jpg)

## Aliasing in PCA

Define VENC as the velocity at which the phase is 180 degrees.

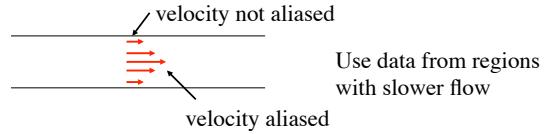
$$VENC = \frac{\pi}{\gamma G_0 T^2}$$

Because of phase wrapping the velocity of spins flowing faster than VENC is ambiguous.



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## Aliasing Solutions



Use multiple VENC values so that the phase differences are smaller than  $\pi$  radians.

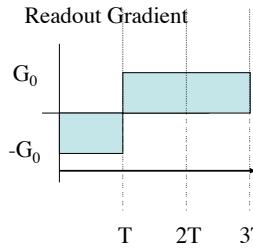
$$\varphi_1 = \pi \frac{v_x}{VENC_1}$$

$$\varphi_2 = \pi \frac{v_x}{VENC_2}$$

$$\varphi_1 - \varphi_2 = \pi v_x \left( \frac{1}{VENC_1} - \frac{1}{VENC_2} \right)$$

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## Flow Artifacts



During readout moving spins within the object will accumulate phase that is in addition to the phase used for imaging. This leads to

- 1) Net phase at echo time TE = 2T.
- 2) An apparent shift in position of the object.
- 3) Blurring of the object due to a quadratic phase term.

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## Flow Artifacts

Plug Flow



All moving spins in the voxel experience the same phase shift at echo time.

Laminar Flow

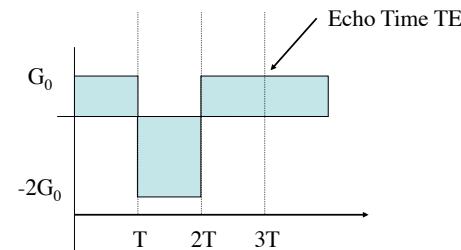


Spins have different phase shifts at echo time. The dephasing causes the cancellation and signal dropout.

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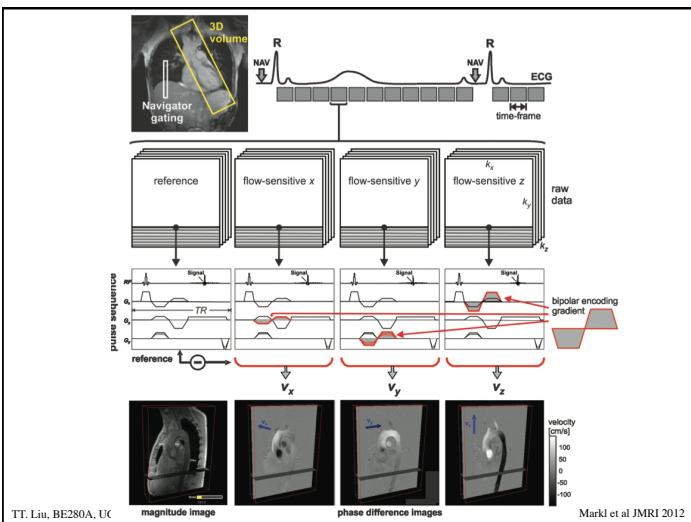
## Flow Compensation

Readout Gradient



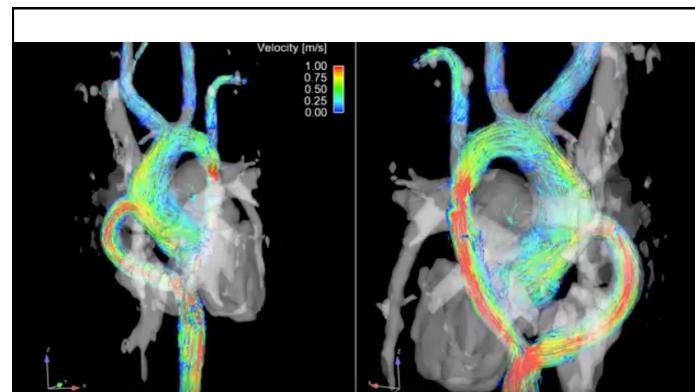
At TE both the first and second order moments are zero, so both stationary and moving spins have zero net phase.

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Markl et al JMRI 2012



<https://www.youtube.com/watch?v=1ORpeB6j0gc>

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## Velocity k-space

A bipolar gradient introduces a phase modulation across velocities of the form  $\varphi(v_x) = -\gamma v_x G_0 T^2$

The MRI signal (with no spatial encoding) acquired across a volume of spins with varying velocities is:

$$\begin{aligned} M(k_{v_x}) &= \int_{-\infty}^{\infty} m(v_x) e^{j\varphi(v_x)} dv_x \\ &= \int_{-\infty}^{\infty} m(v_x) e^{-j\gamma v_x G_0 T^2} dv_x \\ &= \int_{-\infty}^{\infty} m(v_x) e^{-j2\pi k_{v_x} v_x} dv_x \\ &= F[m(v_x)] \text{ with } k_{v_x} = \frac{\gamma}{2\pi} G_0 T^2 \end{aligned}$$

By making measurements with bipolar gradients of varying amplitudes/durations and taking the inverse transform of the measurements, we can obtain the velocity distribution.

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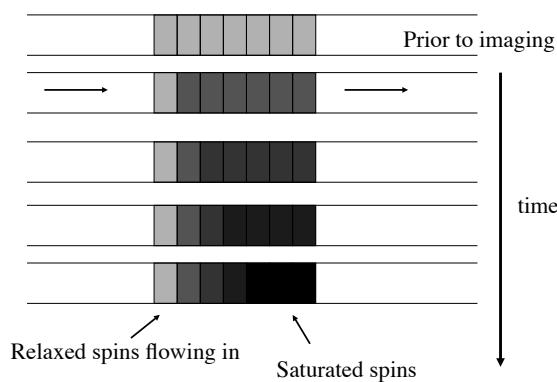
## Velocity k-space

$$M(k_x, k_{v_x}) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} m(x, v_x) e^{-j2\pi k_x x} e^{-j2\pi k_{v_x} v_x} dx dv_x$$

In addition, we can apply imaging gradients so that we can eventually obtain the velocity distribution at each point in space. A full k-space acquisition would then yield 6 dimensions -- 3 spatial dimensions and 3 velocity dimensions.

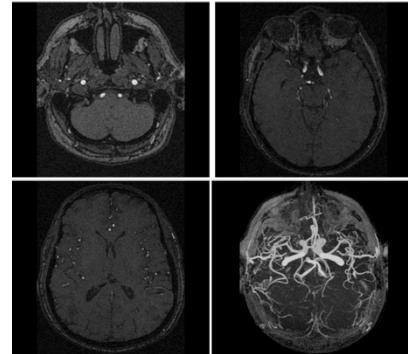
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## Inflow Effect



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## Time of Flight Angiography



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## Cerebral Blood Flow (CBF)

CBF = Perfusion

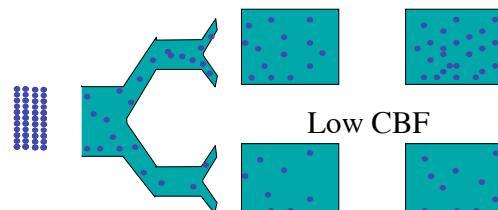
= Rate of delivery of arterial blood to a capillary bed in tissue.

Units: \_\_\_\_\_ (ml of Blood)  
(100 grams of tissue)(minute)

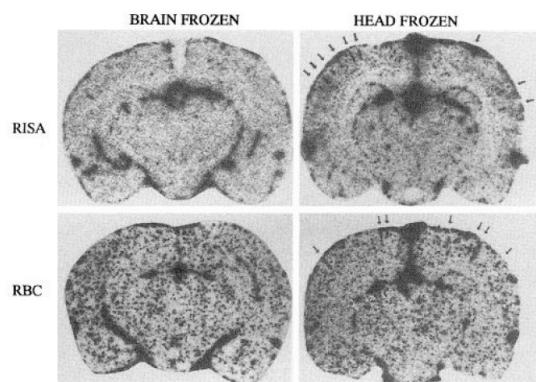
Typical value is 60 ml/(100g-min) or  
60 ml/(100 ml-min) = 0.01 s<sup>-1</sup>, assuming average density of brain equals 1 gm/ml

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High CBF

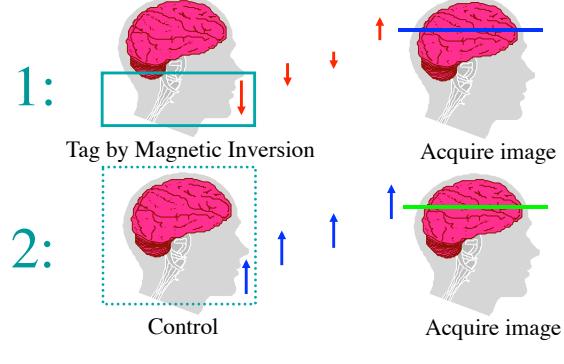


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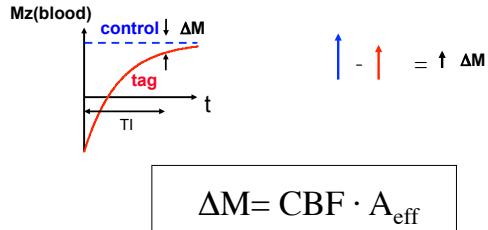
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## Arterial spin labeling (ASL)



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### ASL Signal Equation



$A_{eff}$  is the effective area of the arterial bolus. It depends on both physiology and pulse sequence parameters.

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### ASL Pulse Sequences

PASL / VSASL TR

Tag Acquire Control Acquire

TI = Inversion Time

CASL

Tag Acquire Control Acquire

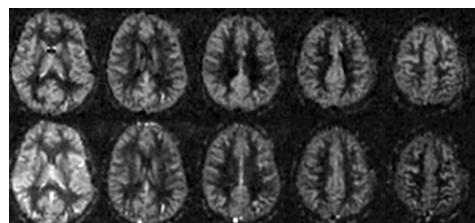
Labeling Time

Post Labeling Delay

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### Multislice CASL and PICORE

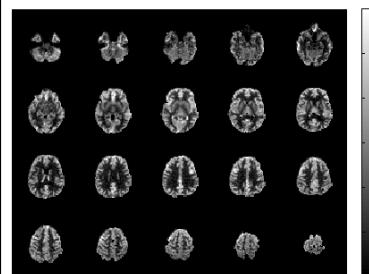
CASL



PICORE  
QUIPSS II

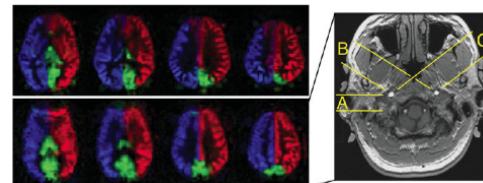
Credit: E. Wong

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Whole brain non-invasive measures of Cerebral Blood Flow obtained with arterial spin labeling (ASL) MRI (Courtesy of D. Shin)

Vascular territory imaging using vessel-encoded ASL (Wong 2007)



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